Calcific lesion preparation for coronary bifurcation stenting

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Abstract

Bifurcating coronary lesions are a very common challenge in interventional cardiology because of the technical complexity in their treatment, the risk of side branch occlusion and an overall worse outcome when compared to non-bifurcating lesions.

The presence of calcifications represents further complexity due to the difficulty in device delivery and stent expansion as well as enhanced risk of side branch occlusion.

Rotational and orbital atherectomy, scoring and cutting balloons, coronary lithoplasty are available tools which have been introduced over the last three decades to overcome such issue. Nevertheless, their application in different contexts of bifurcations presents specific caveats and the studies directed at comparing such techniques have never been expressly oriented in the subset of the bifurcating lesion.

In this paper, we review these devices and their usefulness in bifurcations by analyzing consistent data from clinical trials, and we propose a practical algorithm for the treatment of severely calcified bifurcating lesions according to their anatomical features. (Cardiol J 2019; 26, 5: 429–437)

Key words: bifurcation, calcified lesion, plaque modification, rotational atherectomy, coronary lithoplasty

Introduction

Bifurcating coronary lesions are a very common challenge for interventional cardiologists because of the technical complexity in their treatment, a higher risk of procedural complications and an overall worse outcome compared to non-bifurcating lesions [1]. The inherent difficulty of bifurcation percutaneous coronary intervention (PCI) stems from the risk that main vessel (MV) stenting may hamper flow in the side branch (SB).

The European Bifurcation Club (EBC) consensus document recommends a single “provisional” stenting technique, although acknowledging that bifurcations with diffuse SB involvement often requires double stenting [2]. Several stent techniques have been developed in order to tailor double stent deployment to the complex anatomy of the bifurcation. Hence, significantly higher risk of myocardial infarction and stent thrombosis have been associated with double when compared with single stenting [3].

In this scenario, the main issues to effectively guarantee optimal vessel patency are prevention of plaque shifting and careful carina reconstruction; further complexity may be due to calcification that increases the risk of SB occlusion or hampers crossability or adequate lesion dilatation [4].

Various strategies have been tested in order to prepare the plaque in the bifurcation and to reduce or displace the amount of calcium before stenting, and the inherent scientific literature presents a consistent controversy. The aim of this paper is to review current strategies adopted to modify calcific plaque before stent deployment in coronary bifurcations.
Calcification at bifurcating lesions

When dealing with a bifurcation lesion, the first issue should be an assessment of the relevance of the SB; in this view, Kim et al. [5] clearly documented that a length $\geq 73$ mm, not the diameter of the SB, identifies a vessel supplying a “significant” portion of myocardium, notably a fractional myocardial mass $\geq 10\%$.

Hence, following a widely accepted classification by Medina et al. [6], SB plaque involvement should be checked. The so-called “true bifurcations” define lesions where plaque enters the SB, namely Medina 1,1,1–1,0,1–0,1,1, although there is growing evidence that not the sole SB involvement, but SB lesion length $> 9$ mm is an independent predictor of adverse events [7].

The use of intravascular imaging is of great value to ascertain the distribution of the plaque, the true vessel size and the extent of calcium in bifurcating lesions, even beyond the bifurcation of the left main (LM) [8], that is currently the only site where guidelines recommend the use of intravascular ultrasound (IVUS) [9].

Extensive calcification is the main determinant of balloon and stent underexpansion during PCI (Fig. 1) [10]. The sensitivity of intravascular imaging is far higher than angiography in detecting coronary calcifications, as angiography is able to detect a calcified plaque only for calcium angles almost $> 100^\circ$, by either IVUS or optical coherence tomography (OCT). Nevertheless, all disagreement between the angiography and intravascular imaging is related to thin calcifications that have not been shown to affect stent expansion (Table 1) [4]. Even with the availability of newer drug-eluting stents (DES), patients with severely calcified lesions still have worse clinical outcomes compared with those without [11]. Clinical relevance of coronary calcification cannot be neglected, as treating stent underexpansion in a heavily calcified lesion is more difficult than preventing it [12]. However, although there is general agreement that the greater the arc length, or thickness of calcium, the greater the likelihood of stent underexpansion, there are no published cutoffs that can be used for recommending lesion modification prior to stent implantation or the need for high-pressure adjunctive balloon inflations afterward.

The presence of extensive calcification at the site of bifurcation evaluated by OCT portends a higher risk of occlusion of the side branch, as documented by Fujino et al. [4]. In multivariate analysis, the presence of a calcified plaque in

Table 1. Calcium quantification by imaging modality.

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<tr>
<th>Imaging Modality</th>
<th>Description</th>
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<tr>
<td>Angiography</td>
<td>Radio-opacities before contrast injection noted with cardiac motion (moderate), or without cardiac motion (severe)</td>
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<tr>
<td>Optical coherence tomography</td>
<td>Signal-poor with sharply delineated leading, quantified by thickness (mild $&lt; 0.5$ mm; severe $&gt; 0.5$–1 mm), area, and volume</td>
</tr>
<tr>
<td>Intravascular ultrasound</td>
<td>Hyperechoic leading edge with acoustic shadowing, quantified mainly by angle (concentric if $&gt; 270^\circ$) and length</td>
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Figure 1. Coronary calcified bifurcating lesion. Diffuse calcifications of left anterior descending artery (LAD); A. Fluoroscopy view (arrows indicate calcifications) of LAD; B. Angiographic view; C. Fluoroscopy view of incomplete balloon expansion.
the bifurcation segment of MV (odds ratio [OR]: 12.32; 95% confidence interval [CI]: 2.58–58.83; \( p = 0.002 \)) as assessed by OCT was the most relevant feature associated with SB deterioration, being bifurcation angle > 70° (OR: 11.83; 95% CI: 2.00–70.02; \( p = 0.007 \)) and baseline % diameter of stenosis (DS) of SB (OR 1.07; 95% CI: 1.02–1.13; \( p = 0.012 \)) other independent predictors of SB deterioration, as assessed by angiography.

The mechanism of SB closure due to calcium has not been fully elucidated, but a higher risk of carina shift due to reduced compliance of the wall opposing the SB and a lower resistance encountered by the inflated balloon at the SB ostium could be a potential hypothesis. Carina is typically spared from atherosclerosis distribution owing to high local shear stress [13], but is the potential source of subsequent stent failure. Careful lesion preparation might therefore “soften” the lesion and reduce the risk of plaque shift (Table 2).

### Modifying balloons

The cutting balloon has been available for almost 30 years. It is a semi-compliant balloon with three thin sharp blades mounted on its body, designed to cut the continuity of fibrocalcific plaque once the pressure of the balloon forces them against the vessel wall, creating fissures on the plaque.

The main drawback of these tools is their high rigidity that hinders system advancement and lesion negotiation through tortuous and calcified vessels [14]. Moreover, cutting balloon angioplasty showed a higher rate of coronary perforation (0.8% vs. 0%, \( p = 0.03 \)) and had no advantages in terms of restenosis compared to balloon angioplasty (31% vs. 30%, \( p = \text{NS} \)) [15]. Therefore, after the first optimistic feasibility reports [16], scoring the plaque to facilitate stent deployment has been reported only in occasional cases for treatment of calcified bifurcations. This technology has recently undergone some important revisions: in the newer generation of cutting balloons (Wolverine™ Cutting Balloon, Boston Scientific, USA), the atherotome’s support thickness has been reduced, without affecting the functional height of the blade, resulting in an overall smaller crossing profile and improved crossability.

The principle of using a “buddy wire” to fracture calcified plaque [17] promoted the development of the scoring balloon: wires apposed externally to the body of the balloon increase local punctual pressure, achieving plaque fissuration [18]. Otsuka et al. [19] recently proposed that prolonged inflation might improve the success rate of these devices with a “creep phenomenon”: a sustained tensile load produces microcrack formation and propagation leading to a phasic tissue elongation.

Scoring balloons are available in two different families, the first one is engineered as a traditional balloon with three segments of wire apposed spirally or linearly on the outer surface of the balloon; the second kind has only one external wire and is engineered as a rapid exchange balloon with a very short monorail involving only the tip of the balloon, thus allowing the guidewire to course along the balloon and to serve, together with the other, as a scoring wire. Scoring balloon, especially the latter has a better crossing profile than old generation cutting balloons but still has less deliverability than a standard balloon. Several reports suggest a very good success rate but many authors still consider these devices limited to a less-than-severely calcified lesion.

Using a provisional approach with a scoring balloon for the SB and a DES for the MV in “true” bifurcation lesions yielded promising results in a single arm prospective study, with a rate of crossover to stent deployment in the SB as low as 11%, and a target lesion revascularization rate of 3.3% [20].

### Atherectomy

Rotational atherectomy (RA) (Rotablator, Boston Scientific-Scimed Corporation, Natick, Massachusetts), firstly introduced more than 30 years ago [21], is a plaque modification method achieved by a high-speed diamond chips-coated rotating burr that allows selective abrasion of calcified hard tissues. In the pre-stent era RA was conceived as a stand-alone approach to obtain plaque debulking in order to gain lumen diameter in a severely calcified lesion. It subsequently became evident that RA may offer its best contribution as a major “plaque modifier” for subsequent balloon angioplasty and stent implantation. Calcified ostial and bifurcating lesions were effectively treated by RA in the pre-stent era [22]. Its main effect is to restore adequate lumen by breaking the continuity of calcium plaque, increasing lesion “crossability” and making the artery more compliant to balloon dilatation.

Rotational atherectomy relies on two principles [23]:

- “Differential cutting” defines the ability to selectively ablate hard plaque components while
displacing and sparing soft tissues, that are
deflected away. At rotational speeds > 60,000
rpm the friction, which occurs when sliding
surfaces are in contact, is virtually eliminated.
The “differential cutting” should theoretically
allow RA to accomplish a selective abrasion
of plaque in the proximity of a branch, thus
increasing the procedural success rate and re-
ducing the need for side-branch intervention.
— “Orthogonal displacement of friction” refers
to a change in effective longitudinal friction,
which is almost eliminated, resulting in re-
duced surface drag and unimpeded advance-
ment of the burr in tortuous and diseased
segments of the coronary tree.
Rotablator® advances over a guidewire (Ro-
tawire), is a 325 cm long and 0.009” thin shaft, with
a 0.014” 2.2 cm long floppy spring tip, which has
a lower performance in crossing lesions and tor-
tuosity than a traditional guidewire. Rotawire can
therefore be positioned through a microcatheter
after an exchange with a “workhorse” guidewire.

Table 2. Features of the main plaque modifying devices.

<table>
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<tr>
<th>Device</th>
<th>Material</th>
<th>Technical features</th>
<th>Ref.</th>
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| Focused force dilatation balloon (Scoreflex™) | Semi-compliant or non-compliant balloon            | Balloon size 2.0–4 mm  
Working range 6–16 atm  
Crossing profile 0.032” F  
5F Guiding catheter compatible  
Guide wire 0.014” | [17]    |
| Scoring balloon (Angiosculpt®) | Semi-compliant balloon                             | Balloon size 2.0–3.5 mm  
Working range 2–20 atm  
Crossing profile 0.047” F  
6F Guiding catheter  
Guide wire 0.014” | [17, 20]|
| Cutting balloon (Wolverine™)   | Nylon non-compliant balloon                        | Balloon size 2.0–4.0 mm  
Working range 8–16 atm  
Reduced crossing profile then Flexotome®  
5F Guiding catheter compatible | [16]    |
| Rotational atherectomy (Rotablator®) | Diamond-coated elliptical Burr rotating up to 190,000 rpm | Multiple burrs size (1.25–> 2.5 mm)  
RotaWire™ (330 cm, 0.014”, extra support or floppy)  
Catheter 6–10 F (according to the size burr) | [23]    |
| Orbital atherectomy system (Diamondback 360®) | Eccentrically mounted diamond-coated crown (1.25 mm) rotating up to 200,000 rpm | 6F Guiding catheter  
ViperWire Advance® (0.014”) | [27, 28, 29]|
| Intravascular lithotripsy (Shockwave®) | Semi-compliant balloon containing a series of unfocused, electromechanical lithotripsy emitters | Balloon size 2.5–4 mm  
Inflated to 4 atm and administered 4 cycles of 10 s  
Crossing profile 0.044”  
6F Guiding catheter  
Guide wire 0.014” | [36]    |
The burr is mounted on a spiral drive shaft that is connected to an advancer and covered by a sheath. The burr’s passage through the lesion creates fragments with a diameter theoretically smaller than blood cells; such microparticles should easily cross microcirculation and then be eliminated by the reticuloendothelial system. Nevertheless, the no-reflow phenomenon has frequently been reported after RA-assisted PCI, and therefore the use of a flushing solution containing vasodilators such as calcium antagonists, nitrates or adenosine alone or in combination has been suggested [24]. A widely used solution to cool the Rotablator® turbine and to flush the coronary circulation from debris generated during the ablation is a saline solution with equal proportions of verapamil, nitrates, and heparin (5 mg/5 mg/5,000 U in 500 mL of saline). The use of the Rotablator® is technically demanding and is associated with a significant incidence of adverse events. Among the procedural complications burr’s lodging, coronary perforation, large dissection, acute thrombosis with abrupt coronary occlusion and atroventricular-block have been reported. In order to minimize the complication rate, the EAPCI consensus document [25] recommends distal positioning of the Rotawire in order to have adequate support and stability and the use a rotational speed in the range of 135,000–180,000 rpm to obtain effective plaque modification, with a gentle picking to-and-fro movement of the burr, avoiding brisk deceleration (> 5,000 rpm) and to stop rotation when the burr is over the lesion to minimize the risk of lodgment. During RA procedures the increased quantity of injected contrast medium may cause deterioration of renal function. Therefore, all strategies useful to contain acute kidney injury should be applied [26], although there are no randomized trials exploring this issue.

Currently, as the role of RA has changed from debulking to plaque preparation, a burr-to-artery diameter ratio of 0.5–0.6 (smaller than previously recommended 0.7) should be targeted in order to balance efficacy in lesion ablation and risk of coronary wall damage.

After several failures to cross the lesion, downsizing of the burr is recommended. In case the smallest burr does not pass, a change to a more supportive, or even a larger guiding catheter must be considered.

More recently, the Diamondback 360®, a coronary orbital atherectomy system (OAS) has become available. Mechanism of OAS is a differential sanding to reduce plaque burden with a carbon-coated crown (1.25 mm). Theoretically, softer tissue flexes away from the crown while fibrotic tissue or arterial calcium is engaged. A drive shaft with an eccentrically mounted diamond-coated crown provides proximal and distal sanding; the crown’s orbital diameter expands radially via centrifugal force [27]. Operators can control the speed of rotation, with a higher speed creating a larger sanding diameter by increasing lateral pressure. Pivotal trials have documented safety and feasibility of OAS in preparation of severely calcified plaques before stent deployment [28, 29], although clinical evidence is still limited.

The interest in calcified lesion preparation was recently revived in the Comparison of Strategies to Prepare Severely Calcified Coronary Lesions (PREPARE-CALC) trial, where modifying balloons (cutting or scoring) were compared with RA, in the setting of stable coronary artery disease. Bifurcating lesion were present in 42% of cases. The trial showed a clear superiority in terms of procedural success in the RA group (98% vs. 81%, p < 0.001), driven by a 20% of cross-over to RA, while, at 9 months, mean in-stent late lumen loss was similar in the two groups, as well as stent thrombosis (0% in both groups) [30].

Plaque debulking in coronary bifurcation with any atherectomy device (both RA and OAS) may pose some technical challenges because of the need of single wire use, impeding the protection of side branches (Fig. 2). Reportedly, a tricky approach with a child-in-mother guiding catheter allowed RA with the use of multiple guidewires in order to protect side branches proximal to the target lesion and to gain more support [31].

As for calcified bifurcating lesions, there are several observational studies highlighting the safety and effectiveness of RA, that achieved a high (> 90%) success rate with a low rate of major adverse events (MACE < 5%) and the need for bailout side-branch stenting (< 20%) [32, 33]. Recently, Chambers et al. [34], in a series of patients undergoing atherectomy with either OAS or RA for severely calcified plaques, documented similar low 30-day MACE rates among patients with bifurcation as compared with non-bifurcation lesions. OAS was associated with significantly shorter procedure and fluoroscopy time, as compared with RA.

**Lithoplasty**

Intravascular lithotripsy (IvL) is the most recent tool for the treatment of calcified lesion after being introduced in peripheral vascular angioplasty. IvL consists of a balloon catheter that uses sonic...
Pulses to fracture calcified tissues with virtually no debris production. The concept of acoustic waves to selectively crack hard bodies has been employed in urology for decades. This approach aims to avoid the trauma produced by blades and burrs and their related risk, still offering an effective disruptive action on calcium (Fig. 3).

IvL device is composed of a 12 mm long balloon catheter with three emitters inside the balloon between two radiopaque markers; it has a profile smaller than other modifying balloons, quite comparable to a non-compliant balloon and is available in 7 sizes ranging from 2.5 to 4.0 mm. An electrical discharge at the emitters vaporizes the...
fluid generating a series of sonic pulses that propagate and selectively interact with calcified plaques even in their inner adventitial layer. In the absence of any system mounted onto the balloon itself, the profile of IvL should guarantee better crossability than other modifying balloons, although in severely calcified lesions uncrossable by any balloon, atherectomy seems to stand as a last resource. In another way, unlike RA, IvL can be used with more than a guidewire to protect side branches; its effect might theoretically extend to calcified side branches ostia and, reportedly, it can be used with the kissing balloon technique because of the presumed ability of IvL to propagate across a second balloon. Moreover, IvL has been employed to fracture a calcified plaque outside an underexpanded stent, allowing appropriate stent expansion at subsequent high-pressure dilatation [35]. An OCT study [36] demonstrated that vessel preparation with IvL led to an increase in minimum lumen area and a reduction in area stenosis, allowing stents to be delivered into all target lesions, with an efficacy proportional with calcification severity, with a very low complication rate (no perforation, nor slow/no flow phenomenon). The prospective, multicenter, single arm Study “Disrupt CAD II”, recently documented the safety and the effectiveness of IvL [37].

**Figure 4.** Proposed algorithm for the treatment of severely calcified bifurcating lesions; *Side branch longer than 73 mm, with a diameter ≥ 2 mm; GW — guidewire; MV — main vessel; SB — side branch; PCI-DES — percutaneous coronary intervention–drug-eluting stent.

**Conclusions**

Percutaneous coronary intervention of a severely calcified bifurcating stenosis is a challenge due to the inherent risks related to inadequate stent expansion and side branch compromise. Therefore, adequate lesion preparation with dedicated tools is often required. Modifying balloons are effective in lesion preparation, but their use is undermined by low crossability. Atherectomy, has been available for 30 years only as rotational, more recently it has evolved as orbital, allowing a high success rate, with an increased complication rate as a trade-off. IvL are now promising devices that obtain calcific plaque fragmentation with sonic pulses locally delivered, but the clinical translation of such benefit is still to be determined.

Here we propose a practical algorithm for the treatment of severely calcified bifurcating lesions (Fig. 4); in crossable lesions, modifying balloons, scoring better than cutting, can be the first choice and now IvL is extremely promising. In case of crossing failure, atherectomy still stands as the last resource [38], but it requires SB removal.

**Conflict of interest:** None declared
References


